

# PFM Step-up Battery Charger Controller IC HM4033

# **General Description:**

The J O 6255 is a step up battery charger controller IC which operates from an input voltage of 4V to 28V. The J O 6255 includes on-chip reference voltage, +5V voltage regulator, inductor current sensing, battery voltage monitoring and N-channel MOSSFET driving blocks, etc, which makes the J O 6255 easy to be used with few external components.

The J O 6255 enter charging mode on power up, the external N-channel MOSFET is turned on, when the inductor current rises to the upper limit, the N-channel MOSFET is turned off, then inductor current begins to fall, the energy stored in inductor is transferred to the battery. When inductor current falls to the lower limit, the external N-channel MOSFET is turned on again, and a new cycle starts. Battery voltage is feedback to FB pin via the external resistor divider, when the voltage at FB pin reaches 1.205V(Typical), the charging is terminated, the external N-channel MOSFET remains off until the voltage at FB pin decreases to recharge threshold, The maximum switching frequency of J O 6255 is 1MHz.

J O 6255 adopts 6-pin SOT23 package.

### **Applications:**

- Lithium ion battery charger
- LiFePO4 battery charger
- Lead-Acid battery charger
- Standalone battery charger

### **Features:**

- Input Voltage Range: 4V to 28V
- Inductor Current Sensing
- Battery Voltage Monitoring
- Up to 1MHz Switching Frequency
- Automatic Recharge
- Up to 25W Output Power
- On-Chip Voltage Regulator: 5V, 5mA
- Operating Temperature Range:  $-40^{\circ}$ C to  $85^{\circ}$ C
- 6-Pin SOT23 Package
- Lead-free, rohs-Compliant, Halogen-free

## **Pin Assignment:**





# **Typical Application Circuit:**



Figure 1 Typical Application Circuit



# Figure 2 Block Diagram

# **Block Diagram:**



# **Ordering Information:**

Part No.	Package Type	Pack	<b>Operating Temperature Range</b>		
J O 6255 '"	""""UOT23-6	Tape and Reel, 3000/Reel""	"""""""""""""""""""""""""""""""""""""		

# **Pin Description**

No.	Name	Description		
1	CSN	Negative Input of Inductor Current Sense. A current sense resistor R <sub>CS</sub>		
		between VIN and CSN is needed to sense the inductor current. In normal		
		operation, (VIN-CSN) is between 120mV and 150mV(Typical).		
2	FB	Battery Voltage Feedback Input. Generally, FB pin should be connected to		
		an external resistor divider to monitor the battery voltage. When the voltage at		
		FB pin rises to 1.205V (Typical), the HM4033 enters termination mode, and		
		enters charge mode again if the voltage at FB pin falls below 1.155V(Typical).		
3	VIN	The Positive Terminal of Input Supply. In addition to powering the internal		
		circuits, VIN pin also serves as the positive terminal of inductor current sense.		
4	VCC	+5V Regulator Output. Connect a 4.7uF or 10uF capacitor from VCC to		
		GND, the maximum output current is 5mA.		
5	DRV	Gate Drive Output for External MOSFET. Connect to the gate of an		
		external N-channel MOSFET.		
6	GND	Ground(GND).		

# **ABSOLUTE MAXIMUM RATINGS**

VIN ,CSN to GND	$\dots -0.3$ V to 30V
VCC to GND	0.3V to 6.5V
CSN to VIN	0.3V to 0.3V
FB, DRV	-0.3V to VCC

Maximum Junction Temperature	150°C
Operating Temperature Range40°C	to 85℃
Storage Temperature Range−65°C	to 150°C
Lead Temperature(Soldering, 10S)	260°C

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.



# **ELECTRICAL CHARACTERICS**

Parameters	Symbol	Test Conditions	Min	Тур	Max	Unit
Input Voltage Range	VIN		4		28	V
Switching Frequency	$f_{SW}$				1	MHz
Operating Current	I <sub>VIN</sub>	V <sub>FB</sub> =1.25V, No Switching	395	515	635	uA
Inductor Current Sense C	Comparator					
Sense Threshold High	V <sub>CSHI</sub>	$\begin{array}{l} (\rm VIN-V_{CSN}) \ \ rises \ \ from \ \ 0V, \\ \rm until \ V_{DRV} \ < 0.5V \end{array}$	120	150	180	mV
Sense Threshold Low	V <sub>CSLO</sub>	$(VIN - V_{CSN})$ falls from 0.2V until $V_{DRV} > (VCC - 0.5V)$	96	120	144	mV
Propagation Delay to Output High	t <sub>DPDH</sub>	$(VIN - V_{CSN})$ from 0.2V to 0.07V		82		ns
Propagation Delay to Output Low	t <sub>DPDL</sub>	(VIN $-V_{CSN}$ ) from 0V to 0.2V		82		ns
CSN Input Current	I <sub>CSN</sub>				1	uA
FB Pin						
FB Charge Termination Threshold	V <sub>term</sub>	FB voltage rises	1.19	1.205	1.22	V
FB Recharge Threshold	V <sub>rech</sub>	FB voltage falls	1.13	1.155	1.18	V
FB Current	I <sub>FB</sub>		-100		+100	nA
DRV Pin						
Source Current		$V_{CSN} = VIN, V_{DRV} = 0.5 \times VCC$		0.5		А
Sink Current		$V_{CSN} = VIN - 0.22V,$ $V_{DRV} = 0.5 \times VCC$		1		А
Output Voltage High	V <sub>OH</sub>	I <sub>DRV</sub> =5mA	VCC-0.5		V	
Output Voltage Low	V <sub>OL</sub>	$I_{DRV} = -10 \text{mA}$			0.5	V
VCC Pin						
Regulation Voltage	VCC	$I_{VCC} = 0.1 \text{mA to 5mA},$ VIN=5.5V to 30V	4.5		5.5	V
Load Regulation		$I_{VCC} = 0.1 \text{mA}$ to 5mA,		5		ohm
Line Regulation		VIN=6Vto 28V, $I_{VCC}$ =3mA		6		mV
PSRR	PSRR	$I_{VCC}=3mA$ , $f_{IN}=10kHz$		-35		dB
Start Time	t <sub>START</sub>	VCC = 0 to 4.5V		350		us

(VIN = 12V,  $TA = -40^{\circ}C$  to +85°C, Typical values are at TA = +25°C, unless otherwise noted)

# **Detailed Description**

The HM4033 is a step up battery charger controller IC which operates from an input voltage of 4V to 28V. The HM4033 includes an on-chip reference voltage, +5V voltage regulator, inductor current sensing, battery voltage monitoring and N-channel MOSFET driving blocks, etc, which makes the HM4033 easy to be used with few external components.

The HM4033 enters charge mode on power up, the external N-channel MOSFET is turned on, inductor current rises. When the inductor current rises to the upper limit, the N-channel MOSFET is turned off, and inductor current begins to fall, the energy stored in inductor is transferred to the battery. When inductor current falls to the



lower limit, the external N-channel MOSFET is turned on again, and a new cycle starts. Battery voltage is feedback to FB pin via the external resistor divider, when the voltage at FB pin rises to 1.205V(Typical), the charging is terminated, the external N-channel MOSFET remains off until the voltage at FB pin decreases to recharge threshold, which will make HM4033 enter charge status again. The maximum switching frequency of HM4033 can be up to 1MHz.

# **Application Information**

### About Input Voltage Range

HM4033 operates from a 4V to 28V input voltage. When the input voltage is between 4V to 5.5V, the voltage at VCC pin may be less than 5V, though HM4033 can function correctly.

### **5V Voltage Regulator**

VCC is the output of a 5V regulator capable of sourcing 5mA. Bypass VCC to GND with a  $4.7\mu$ F to  $10\mu$ F capacitor.

### **Inductor Current (Input Current)**

In the application circuit shown in Figure 1, HM4033 sets the inductor current through a current sense resistor  $R_{CS}$  connected between VIN and CSN pin.

When the external N-channel MOSFET is turned on, inductor current rises, when inductor current rises to:

$$I_{Lhigh} = 0.15 V / R_{CS}$$

The external N-channel MOSFET is turned off, inductor current falls, and the energy is transferred to the battery and the output capacitor. When inductor current falls to:

$$I_{Llow} = 0.12 V / R_{CS}$$

The external N-channel MOSFET is turned on again, and a new cycle begins.

So, average inductor current is:  $I_L = 0.135 V / R_{CS}$ 

In the above 3 equations, I<sub>Lhigh</sub> is upper limit of inductor current in ampere(A)

I<sub>Llow</sub> is lower limit of inductor current in ampere(A)

 $R_{CS}$  is current sense resistor in ohm(  $\Omega$  )

### **Calculate Switching Frequency and Duty Cycle**

In the application circuit shown in Figure 1, the on-time of external N-channel MOSFET is:

$$ton = \frac{0.03 \text{ X L}}{\text{VIN X Rcs}}$$

The off-time of external N-channel MOSFET is:

$$t \circ ff = \frac{0.03 \times L}{(V_{BAT} + V_D - V_{IN}) \times R_{CS}}$$

Switching frequency is:

$$f_{sw} = \frac{1}{ton + toff} = \frac{1}{\frac{0.03 \times L}{VIN \times Rcs} + \frac{0.03 \times L}{(VBAT + VD - VIN) \times Rcs}}$$

Duty cycle is:

$$D = \frac{ton}{ton + toff} = \frac{V_{BAT} + V_D - VIN}{V_{BAT} + V_D}$$

In the above 4 equations, L is inductor value in Henry(H)



VIN is input voltage in Volt(V)

 $V_{BAT}$  is battery voltage in Volt(V)

 $V_D$  is the forward voltage of diode D1 in Volt(V)

 $R_{CS}$  is inductor current sense resistor in ohm(  $\Omega$  )

### **Estimate Charge Current**

HM4033 controls the charge current by controling inductor current(Input current), so the charge current will vary with the input voltage and battery voltage.

Generally, the charge current can be estimated by the following equation:

$$I_{CH} = \frac{VIN X I_L \chi \eta}{V_{BAT}}$$

Where,

I<sub>CH</sub> is the charge current in Ampere (A) VIN is input supply in Volt(V)

 $I_L$  is average inductor current, which is determined by 0.135 /  $R_{CS}$  in Ampere(A)

 $\eta$  is converter's efficiency, which is around 85%

 $V_{BAT}$  is battery voltage in Volt(V)

### **Charge Termination Voltage at Battery Terminal**

In the application circuit shown in Figure 1, battery voltage is feedback to FB pin via the resistor divider formed by R1 and R2, HM4033 decides the charge status based on FB's voltage. When FB voltage rises to 1.205V (Typical), HM4033 enters termination mode.

The voltage at battery terminal when the charging is terminated:

$$V_{BAT} = 1.205 \times (1 + R1 / R2)$$

Since R1 and R2 will draw some current from the battery, R1+R2 should be chosen first according to the current consumption affordable, then calculate R1 and R2 based on the above equation.

When designing the charge termination voltage at the battery terminal, the battery's internal resistance and the parasitic resistance from the PCB to the battery's terminals should be taken into consideration. As illustrated in Figure 3,  $R_B$  is the battery's internal resistance,  $R_W$  is the parasitic resistance including the metal wire's resistance, plug contact resistance, etc.



## Figure 3 Battery's Internal Resistance and Parasitic Resistance

In charge mode, charge current flows through the resistor  $R_B$  and  $R_W$ , a voltage drop  $V_R$  is generated. Assume that the true battery voltage is  $V_{BAT}$ , but the detected voltage by HM4033 is  $V_{BAT} + V_R$ , which does not accurately reflect the battery voltage. Therefore, when designing the charge termination voltage, the voltage drop  $V_R$  should be considered to make sure that the battery is fully charged.

The simple way to compensate  $V_R$  is to make:

 $V_{final} = V_{BAT} + V_R$ 

Where,  $V_{\text{final}}$  is the designed charge termination voltage at battery terminal

 $V_{BAT}$  is battery voltage when fully charged



V<sub>R</sub> is the voltage drop across the battery's internal resistance and parasitic resistance

#### **Charge Termination**

When the voltage at FB pin rises to 1.205V (Typical), the charging is terminated, the external N-channel MOSFET is turned off, HM4033 is in charge termination status, in which there is no charge current flowing to the battery.

### Recharge

In charge termination mode, if FB voltage falls to 1.155V(Typical), HM4033 will enter charge mode again.

### **MOSFET Selection**

The HM4033's gate driver is capable of sourcing 0.5A and sinking 1A of current. MOSFET selection is based on the maximum battery voltage, inductor current and operating switching frequency. Choose an N-channel MOSFET that has a higher breakdown voltage than the maximum battery voltage, low Rds(ON), and low total gate charge(Qg) for better efficiency. MOSFET threshold voltage must be adequate if operated at the low end of the input-voltage operating range.

### **Freewheeling Diode Selection**

The forward voltage of the freewheeling diode should be as low as possible for better efficiency. A Schottky diode is a good choice as long as the breakdown voltage is high enough to withstand the maximum battery voltage. The forward current rating of the diode must be at least equal to the maximum charge current.

### **Input Bypass Capacitor**

In most applications, a bypass capacitor at VIN is needed. An at least 1uF ceramic capacitor, placed in close proximity to VIN and GND pins, works well. In some applications depending on the power supply characteristics and cable length, it may be necessary to increase the capacitor's value. The capacitor's breakdown voltage should be higher than the maximum input voltage.

### **Output Capacitor**

An at least 10uF capacitor is needed between output and ground(GND).

### **About Capacitor C3**

In the typical application circuit shown in Figure 1,capacitor C3 is used to filter out the high frequency noise so that the charger can be terminated correctly. Capacitor C3 is estimated by the below equation:

$$C3 = \frac{5\Pi}{\mathbf{f}_{SW} \times \frac{R1R2}{R1+R2}}$$

Where,

- $\Pi$  is equal to 3.14
- $f_{SW}$  is the converter's switching frequency
- R1 and R2 are the feedback resistors shown in Figure 1

C3's capacitance can not be much larger than the value calculated from the above equation, otherwise the output voltage may go so high that damage may be caused when the battery is absent.

### **Add Charging Status Indication**

The following circuit can be used to add charging status indication and termination status indication.





Figure 4 Charging Status Indication

Where, HM4033 DRV is HM4033's DRV pin, VIN is the charger's input voltage. LED1 is for charging status indication, LED2 is for termination indication. R1 and R2 are the LED current limit resistors.

### **Design Procedure**

The following procedure should be followed to design HM4033's application circuit:

- (1) Decide charge current based on the battery capacity and charge time
- (2) Estimate average inductor current based on input voltage, battery voltage and charge current
- (3) Decide  $R_{CS}$  based on average inductor current
- (4) Determine the inductor value based on the switching frequency
- (5) Design resistor divider formed by R1 and R2 for battery voltage feedback
- (6) Calculate capacitance of C3

### **PCB** Considerations

Careful PCB layout is critical to achieve low switching losses and stable operation.

- Use a multilayer board whenever possible for better noise immunity.
- The negative terminals of input bypass capacitor and output capacitor should be as close as possible to the source of N-channel MOSFET
- The analog ground should be separated with power ground plane.
- To ensure low EMI, the copper plane for diode, N-channel MOSFET, inductor, input capacitor and output capacitor should be as small as possible,
- The current sense resistor R<sub>CS</sub> should be placed closely to input bypassing capacitors.



# **Package Information**

